

# ECE 207 Elements of Electrical Engineering II

## Final Exam

Name\_\_\_\_\_

Campus Mail\_\_\_\_\_

For full credit: 1)work neatly, 2)give appropriate units on answers, and  
3)clearly show all your work.

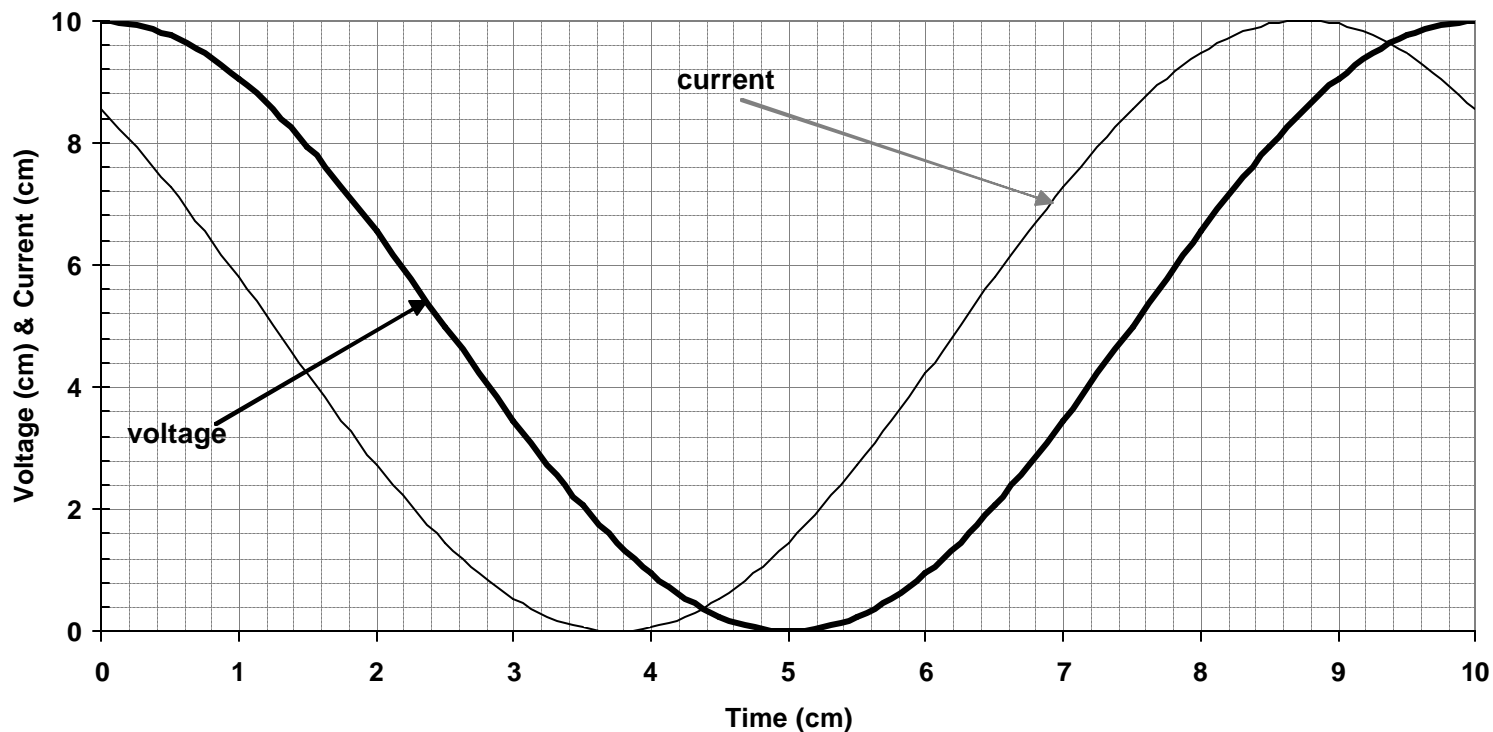
Laptops and two 2-sided 8½"x11" sheets permitted.

$$1 \text{ hp} = 746 \text{ W}, \mu_0 = 4\pi(10^{-7}) \text{ H/m}$$

question	possible points	awarded points
1	25	
2	25	
3	25	
4	25	
5	25	
6	25	
7	25	
8	25	
Total	200	

1. A trace from an oscilloscope is shown below. The voltage channel was set on 10 V/cm, while the current channel was set on 2 A/cm. The time-base was set at 1 msec/cm. Determine:
  - i) The phasors for voltage and current (in RMS).
  - ii) Complex power associated with the circuit.
  - iii) Power factor associated with the circuit (be sure to indicate lag or lead).
  - iv) Frequency (Hz) of the supply.
  - v) Impedance of the circuit (assume elements are in series).

### Oscilloscope Trace of Voltage & Current



2. A 1 $\phi$  transformer is rated 500 kVA, 7200 V : 600 V and has the following approximate equivalent circuit parameters referred to the high voltage side:

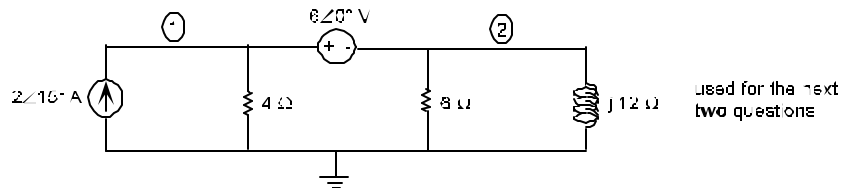
$$R = 2.5 \, \Omega, \quad X = 5 \, \Omega, \quad R_c = 4000 \, \Omega, \quad X_m = 3000 \, \Omega$$

Determine the Voltage Regulation and Efficiency when rated load is supplied at 600V and 0.8 **leading** pf.

3. A three-phase, 60 Hz, Y-connected source is connected to a Y-connected load through a three-phase feeder. The three-phase load draws 900 kW at a 0.8 lagging power factor. The feeder has an impedance of  $0.5 + j1.5 \text{ } \Omega/\text{phase}$ . The voltage at the load is 13.8 kV. Determine:
- i) Phase a line and phase voltages at the load (use  $\mathbf{V}_{an}$  at the load as reference)
  - ii) Phase a line and phase currents (use  $\mathbf{V}_{an}$  at the load as reference)
  - iii) Three-phase average power delivered by the source
  - iv) Capacitance ( $\mu\text{F}/\text{phase}$ ) of a capacitor to improve the power factor to unity at the load
  - v) The magnitude of new line current after the power factor correction

4. Mark **each** true/false question either **T** OR **F** (2 pts each)

\_\_\_ Given a circuit with 7 nodes and 2 voltage sources, the number of KCL equations necessary when performing nodal analysis will be 5.



used for the next two questions

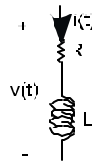
\_\_\_ The nodal equations are  $\frac{\tilde{V}_1}{4\Omega} + \frac{\tilde{V}_2}{6\Omega} + \frac{\tilde{V}_2}{j12\Omega} = 2\angle 15^\circ \text{ A}$  and  $\tilde{V}_1 - \tilde{V}_2 = 6\angle 0^\circ \text{ V}$

\_\_\_ The average power delivered by the voltage source is  $\text{Re} \left[ (6\angle 0^\circ \text{ V}) \left( \frac{\tilde{V}_1}{4\Omega} - 2\angle 15^\circ \text{ A} \right) \right]$

Why or why not? \_\_\_\_\_

$$v(t) = \sqrt{2}(20) \cos(377t) \text{ V}$$

$$i(t) = 60 \cos(377t - 15^\circ) \text{ A}$$



used for the next two questions

\_\_\_  $R = 2 \Omega$  and  $L = 2/377 \text{ H}$ .

\_\_\_ The power absorbed is  $P = 3.6 \text{ kW}$  and the power factor is  $\frac{1}{\sqrt{2}}$  lagging.

Why or why not? \_\_\_\_\_

\_\_\_ Given two loads, both with lagging power factors: the one with the lowest pf requires a pf correction capacitor with a larger value in Farads to correct the power factor to 1.

\_\_\_ In a balanced 3 $\phi$  system, if  $\tilde{V}_{ab} = 120\angle 30^\circ \text{ V}$  and  $\tilde{I}_a = 4\angle 0^\circ \text{ A}$ , then the pf=1 and  $P_{3\phi} = \sqrt{3}(120)(4)\text{W}$ .

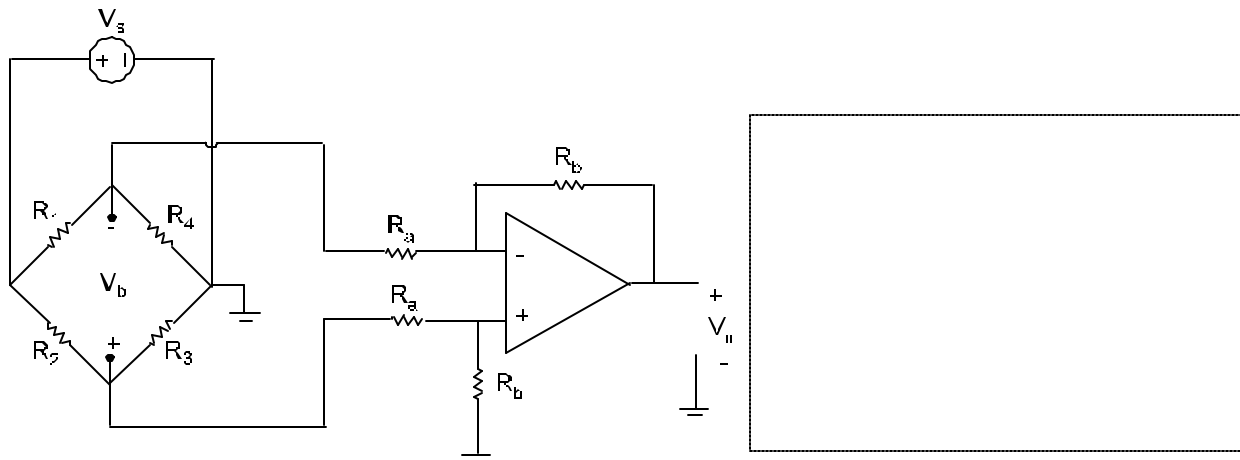
\_\_\_ Given two induction motors, both with the same rated speeds and efficiencies: Motor 1 is rated 480V, 10A. Motor 2 is rated 240V, 20A. Motor 1 and motor 2 have the same rated output power and the same rated torques.

\_\_\_ The rated speed of an induction motor is 3480 rpm. Assuming a 60Hz power system, this motor must be a 2-pole motor and if connected to a load requiring  $\frac{1}{4}$  its rated torque, the speed of the motor-load combination will be 3510 rpm.

\_\_\_ A low-pass filter with  $\omega_b = 1000 \text{ rad/s}$  and a DC gain of 10 has a transfer function of  $\frac{10}{s + 1000}$  and its

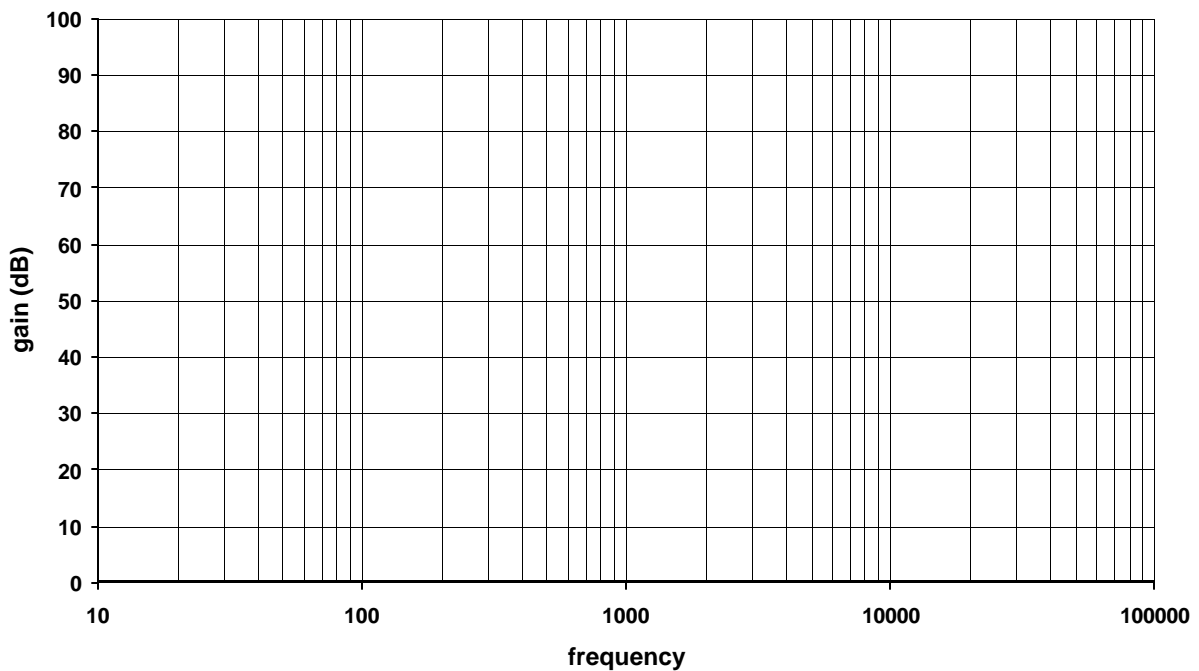
time-domain response to an input of  $1u(t) \text{ V}$  is  $10 \left( 1 - e^{-t/1000} \right) \text{ V}$ .

5. i) When a given load is placed on a **four-active arm** cantilever load cell,  $\epsilon=0.0002$ .  
 $S=2$ ,  $V_s=15V$ ,  $R_1, R_2, R_3$ , and  $R_4$  are  $350\Omega$  strain gages. Use  $R_a = 1\text{ k}\Omega$
- What is  $V_b$ ?
  - Specify the amplifier below to give an output of  $V_o=60\text{ mV}$  for these conditions.



- ii) A filtering stage is needed. Design an active **lowpass** filtering stage to filter  $V_o$  with  $\omega_b=1000$  r/s and a gain of 20dB. Use  $C = 0.01\text{ mF}$  Neatly add this stage to the above schematic.

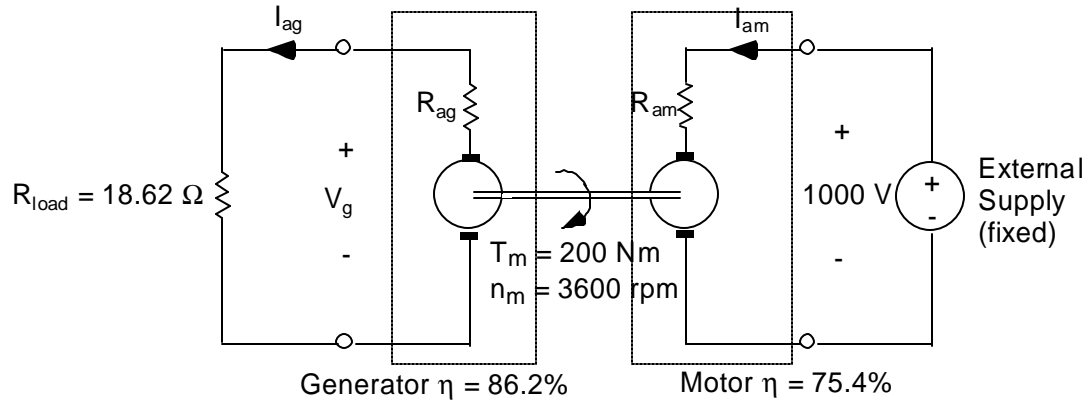
- iii) Neatly sketch the straight line Bode magnitude plot for  $|V_{\text{out-bp filter}}/V_b|$



6. The system below consists of a separately excited DC motor-generator set. The field windings are

not shown. Determine:

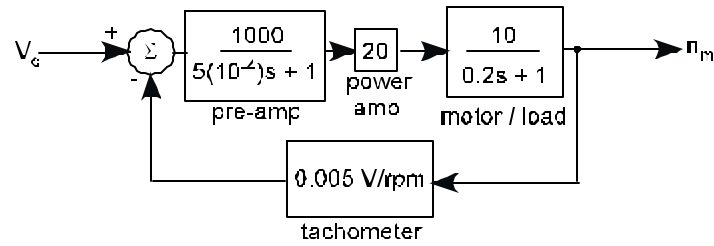
- i) the current at the motor input,  $I_{am}$
- ii) the power delivered to  $R_{load}$
- iii) the load voltage  $V_g$



- iv) Suppose the motor field current was increased (generator field current and  $R_{load}$  remains constant). Explain (in words) what affect would this have on each of the following:
  - the shaft speed,  $n_m$
  - the power delivered to  $R_{load}$
  - the shaft torque,  $T_m$
  - the motor input current,  $I_{am}$

7. For the shown DC motor speed control system, determine:

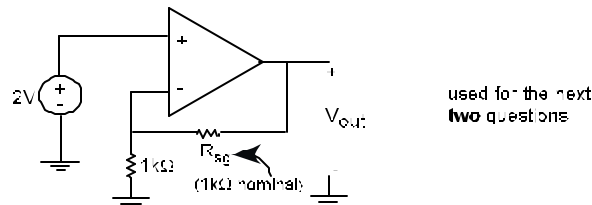
- i) The ideal closed-loop gain
- ii) The exact closed-loop gain in polynomial form
- iii) Compare the steady-state values of parts i) and ii) by calculating the % Error (use the ideal value as your reference)





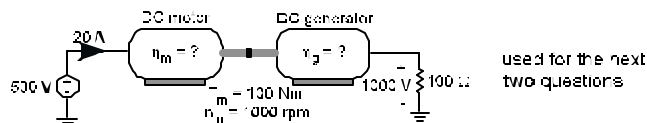
8. Mark **each** true/false question either **T** OR **F** (2 pts each)

\_\_\_ The advantage of RTDs is that they can reliably measure higher temperatures than any type of thermocouple.



\_\_\_ An ideal op-amp is used to measure strain as shown above. Given a nominal  $1k\Omega$  resistance for the strain gage, and a strain gage factor of 2,  $v_{out} = 4.004V$  if the strain,  $\epsilon=0.001$ .

\_\_\_ Given the same strain gage,  $v_{out} = 4 \cos 10t$  mV if the strain,  $\epsilon=0.001 \cos(10t)$ .

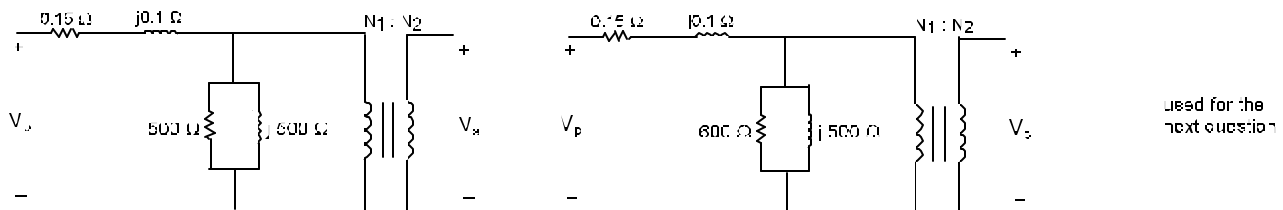


NUMERIC  $\eta_m = \underline{\hspace{2cm}}$  and  $\eta_g = \underline{\hspace{2cm}}$ .

\_\_\_ These efficiencies are not possible.

**Why or why not?** \_\_\_\_\_

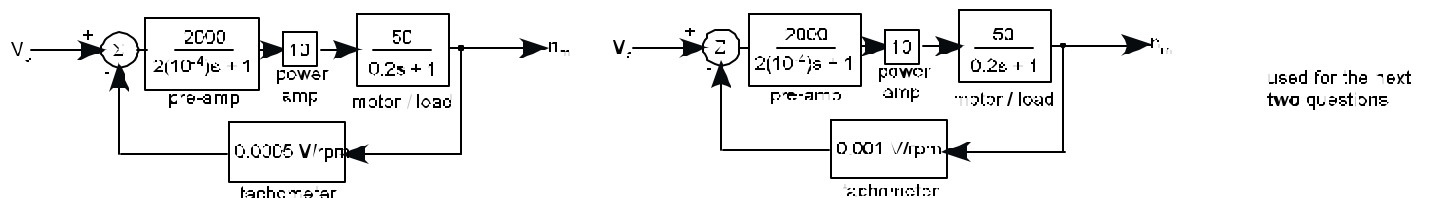
\_\_\_ Time and frequency domain. Lowering the break frequency of a low-pass filter will allow it, in its time-domain response to a step function input, to reach its steady-state value more quickly.



\_\_\_ The two transformers are identical apart from different  $R_c$ . The transformer on the left will be more efficient.

**Why or why not?** \_\_\_\_\_

\_\_\_ The unit step-response for a 2<sup>nd</sup>-order system is  $40 - e^{-100.5t}(\cos 1000t + 0.1005\sin 1000t)$ . If  $\zeta$  were increased (same value of  $\omega_n$  and still underdamped), the frequency of oscillations in the transient response would be lower and the transient response would die out more quickly.



\_\_\_ Given identical inputs, the steady-state speed of the motor in the left system will be lower than that of the right.

\_\_\_ If the motor/load transfer function in the system on the left were changed to  $100/(0.2s+1)$ , the steady-state speed of its motor/load would be doubled for a given  $V_c$ .

**Why or why not?** \_\_\_\_\_

# ANSWERS

1. Note the voltage and current waveforms are given in cm with conversion factors.
  - i)  $V = 35.36\angle 0^\circ \text{ V}$ ,  $I = 7.07\angle 44.64^\circ \text{ A}$ , ii)  $S = 250\angle -44.64^\circ \text{ VA}$ , iii) 0.7 lead,
  - iv) 100 Hz, v)  $Z = (3.56 - j3.51) \Omega$ ,  $[R = 3.56 \Omega, C = 453.4 \mu\text{F}]$
  
2. Note that, for leading pf, %VR can be negative.
 

% VR = -0.825%, % $\eta$ =94.2%
  
3.
  - i) That is, find  $V_{ab}$  and  $V_{an'}$  at the load.  
 $V_{an'} = 7967.4\angle 0^\circ \text{ V}$ ,  $V_{ab} = 13800\angle 30^\circ \text{ V}$
  - ii)  $47.1\angle -36.9^\circ \text{ A}$
  - iii)  $P_{3\phi} = 903.3 \text{ KW}$
  - iv)  $9.4 \mu\text{F}$
  - v)  $37.7 \text{ A}$
  
4. F, T, F, T, T, T, T, T, F, F
  
5. 6 mV, 11.75 k $\Omega$ 
  - ii)  $R_{in} = 10 \text{ k}\Omega$ ,  $R_f = 100 \text{ k}\Omega$
  - iii) LP, break frequency at 1000 r/s, LF gain is 40 dB (20 dB from diff. amp and 20 dB from LP filter)
  
6. Note motor and generator efficiencies
  - i) 100 A
  - ii) 65 kW
  - iii) 1100 V
  - iv) *note that  $E_{am}$  will remain relatively constant*
    - $n_m$  decreases which will cause generator voltage to drop
    - power to the load will therefore drop as approximately the square of the generator voltage
    - $T_g = T_m$  will be reduced because of the lower generator current
    - Since  $T_m$  is reduced even as  $\phi_m$  is increased,  $I_{am}$  must reduce approximately quadratically
  
7.
  - i) 200 rpm/V
  - ii)  $\frac{200000}{10^{-4} \text{ s}^2 + 0.2005 \text{ s} + 1001}$
  - iii) -0.1%
  
8. F, T, F, T, F, F, T, F, F