

Name Solutions CM _____

ECE-205

Exam 3

Fall 2012

Calculators and computers are not allowed. You must show your work to receive credit.

Problem 1 _____ /20

Problem 2 _____ /15

Problem 3 _____ /15

Problem 4 _____ /20

Problems 5 _____ /30

Total _____

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1) (20 points) For the following transfer functions, determine the unit step response of the system. *Do not forget any necessary unit step functions.*

a) $H(s) = \frac{e^{-2s}}{s}$

b) $H(s) = \frac{1}{(s+1)^2}$

c) $H(s) = \frac{1}{s^2 + 2s + 5}$

a) $Y(s) = H(s) \frac{1}{s} = \frac{e^{-2s}}{s^2}$ $y(t) = (t-2)u(t-2)$

b) $Y(s) = H(s) \frac{1}{s} = \frac{1}{s(s+1)^2} = \frac{a_1}{s} + \frac{a_2}{s+1} + \frac{a_3}{(s+1)^2}$ $a_1 = 1 \quad a_3 = -1$
 $\text{as } s \rightarrow \infty \quad 0 = a_1 + a_2$
 $a_2 = -a_1 = -1$

$y(t) = [1 - e^{-t} - t e^{-t}]u(t)$

c) $Y(s) = H(s) \frac{1}{s} = \frac{1}{s[(s+1)^2 + 4]} = \frac{A}{s} + B \left[\frac{2}{[(s+1)^2 + 2^2]} \right] + C \left[\frac{s+1}{[(s+1)^2 + 4]} \right]$

$A = \frac{1}{s} \quad \text{as } s \rightarrow \infty \quad 0 = A + C \quad C = -\frac{1}{5}$

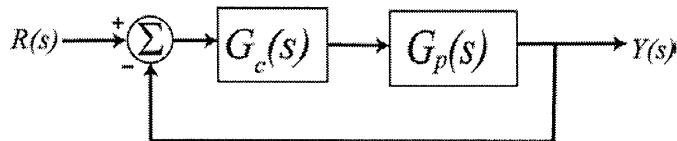
let $s = -1 \quad -\frac{1}{4} = -\frac{1}{s} + \frac{B}{2}$

$-s = -4 + 10B$

$-1 = 10B \quad B = -\frac{1}{10}$

$y(t) = \left[\frac{1}{s} - \frac{1}{10} e^{-t} \sin(2t) - \frac{1}{5} e^{-t} \cos(2t) \right] u(t)$

2) (15 points) Consider the following simple feedback control block diagram. The plant, the thing we want to control, has the transfer function $G_p(s) = \frac{5}{s+3}$



- a) Determine the settling time of the plant alone (assuming there is no feedback)

$$T_s = \frac{4}{3}$$

- b) Determine the steady state error for plant alone assuming the input is a unit step (simplify your answer)

$$e_{ss} = 1 - G_p(0) = 1 - \frac{5}{3} = -\frac{2}{3} = e_{ss}$$

- c) For a proportional controller, $G_c(s) = k_p$, determine the closed loop transfer function $G_0(s)$

$$G_0(s) = \frac{5k_p}{s+3+5k_p}$$

- d) Determine the settling time of the closed loop system, in terms of k_p

$$T_s = \frac{4}{3+5k_p}$$

- e) Determine the steady state error of the closed loop system for a unit step, in terms of k_p (simplify your answer)

$$e_{ss} = 1 - G_0(0) = 1 - \frac{5k_p}{3+5k_p} = \frac{3}{3+5k_p} = e_{ss}$$

- f) For an integral controller, $G_c(s) = \frac{k_i}{s}$, determine the closed loop transfer function $G_0(s)$ and the steady state error for a unit step in terms of k_i

$$G_0(s) = \frac{\frac{k_i}{s} \cdot \frac{5}{s+3}}{1 + \frac{k_i}{s} \cdot \frac{5}{s+3}} = \frac{5k_i}{s^2 + 3s + 5k_i} = G_0(s)$$

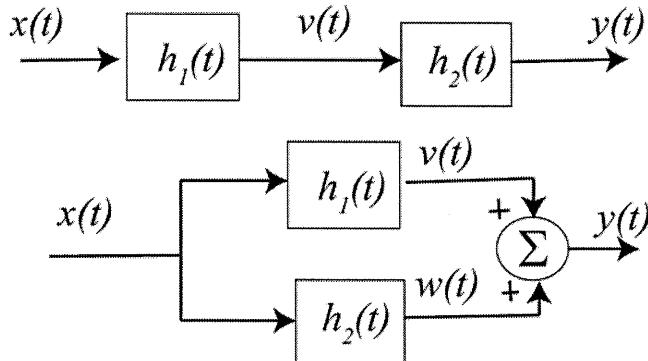
$$e_{ss} = 1 - G_0(0) = 1 - 1 = 0 = e_{ss}$$

3) (15 points) For the following block diagram

For the following interconnected systems,

i) determine the overall impulse response (the impulse response between input $x(t)$ and output $y(t)$) and

ii) determine if the system is causal.



a) $h_1(t) = \delta(t-2)$, $h_2(t) = \delta(t+1)$

b) $h_1(t) = u(t+1)$, $h_2(t) = u(t-2) + \delta(t-2)$

Series Connections:

$$\begin{aligned} a) h_{1+2}(t) &= h_1(t) * h_2(t) = \int_{-\infty}^{\infty} h_1(t-\lambda) h_2(\lambda) d\lambda = \int_{-\infty}^{\infty} \delta(t-\lambda-2) \delta(\lambda+1) d\lambda = [S(t-1)] \boxed{\text{causal}} \\ b) h_{1+2}(t) &= h_1(t) * h_2(t) = \int_{-\infty}^{\infty} h_1(t-\lambda) h_2(\lambda) d\lambda = \int_{-\infty}^{\infty} u(t-\lambda+1) u(\lambda-2) d\lambda + \int_{-\infty}^{\infty} u(t-\lambda+1) \delta(\lambda-2) d\lambda \\ &= \int_2^{t+1} u(\lambda-1) d\lambda + u(t-1) = [(t-1)u(t-1) + u(t-1)] \boxed{\text{causal}} \\ &= t u(t-1) \end{aligned}$$

Parallel Connections:

$$\begin{aligned} a) h_{1+2}(t) &= h_1(t) + h_2(t) = [S(t-2) + S(t+1)] \boxed{\text{not causal}} \\ b) h_{1+2}(t) &= h_1(t) + h_2(t) = [u(t+1) + u(t-2) + S(t-2)] \boxed{\text{not causal}} \end{aligned}$$

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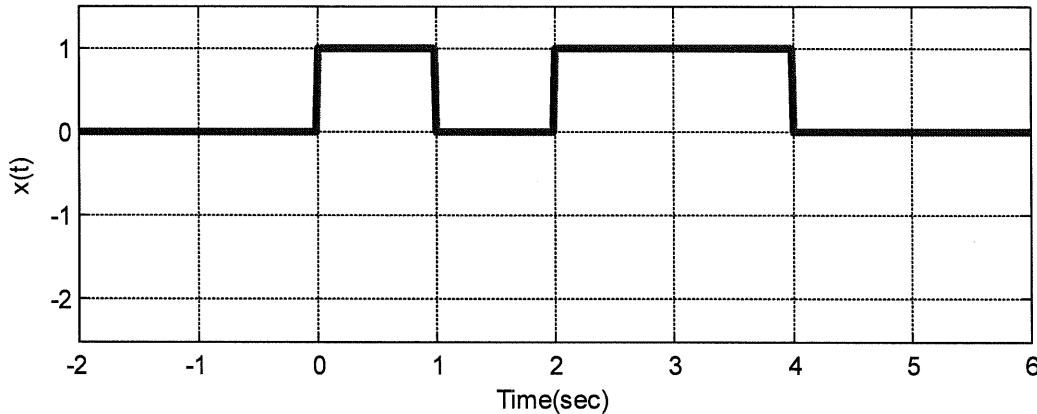
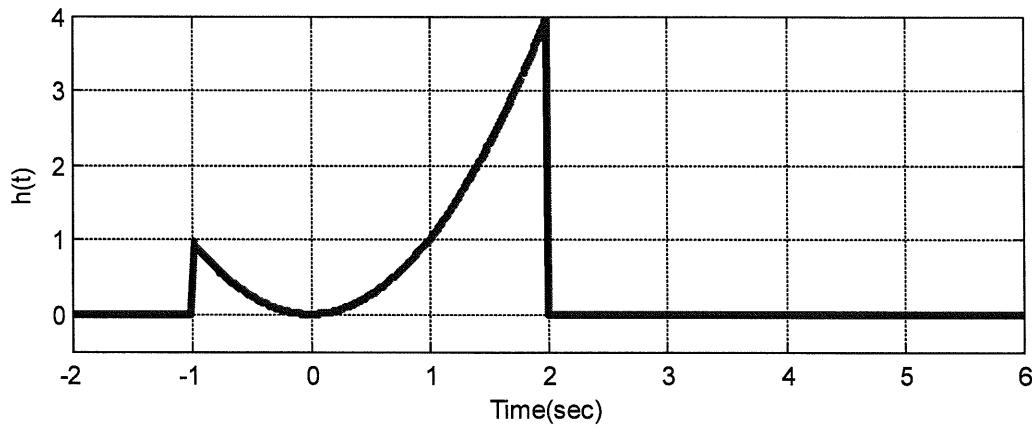
4) (20 points) Consider a linear time invariant system with impulse response given by

$$h(t) = t^2[u(t+1) - u(t-2)]$$

The input to the system is given by

$$x(t) = [u(t) - u(t-1)] + [u(t-2) - u(t-4)]$$

The impulse response and input are shown below:

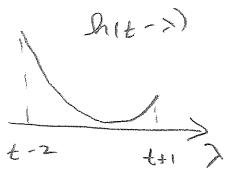


Using **graphical evaluation**, determine the output $y(t)$. Specifically, you must

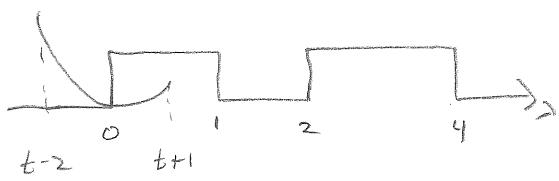
- Flip and slide $h(t)$, NOT $x(t)$
- Show graphs displaying both $h(t - \lambda)$ and $x(\lambda)$ for each region of interest
- Determine the range of t for which each part of your solution is valid
- Set up any necessary integrals to compute $y(t)$. Your integrals must be complete, in that they cannot contain the symbols $x(\lambda)$ or $h(t - \lambda)$ but must contain the actual functions.
- Your integrals cannot contain any unit step functions
- **DO NOT EVALUATE THE INTEGRALS!!**

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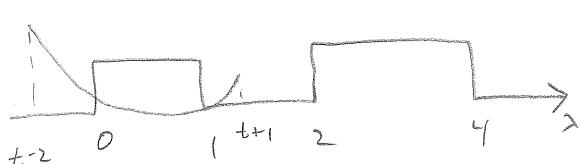
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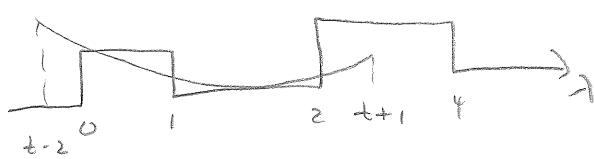
$$y_1(t) = 0 \quad t < -1$$



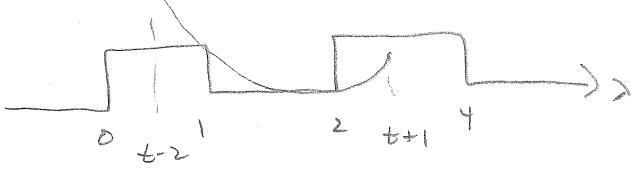
$$-1 \leq t \leq 0 \quad y_1(t) = \int_0^{t+1} (t-\lambda)^2 d\lambda$$



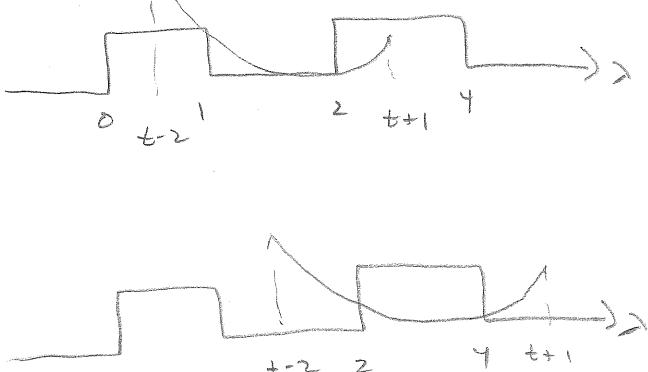
$$0 \leq t \leq 1 \quad y_1(t) = \int_0^1 (t-\lambda)^2 d\lambda$$



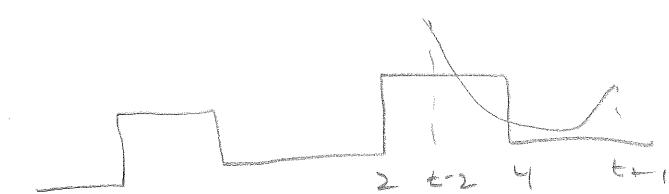
$$1 \leq t \leq 2 \quad y_1(t) = \int_0^1 (t-\lambda)^2 d\lambda + \int_2^{t+1} (t-\lambda)^2 d\lambda$$



$$2 \leq t \leq 3 \quad y_1(t) = \int_{t-2}^1 (t-\lambda)^2 d\lambda + \int_2^{t+1} (t-\lambda)^2 d\lambda$$



$$3 \leq t \leq 4 \quad y_1(t) = \int_2^4 (t-\lambda)^2 d\lambda$$



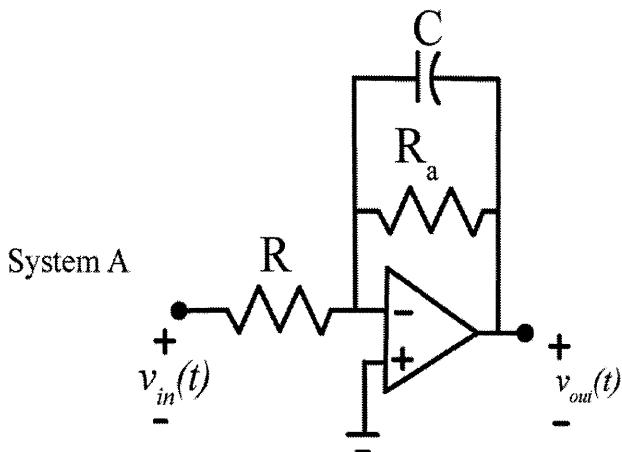
$$4 \leq t \leq 6 \quad y_1(t) = \int_{t-2}^4 (t-\lambda)^2 d\lambda$$

$$t \geq 6 \quad y_1(t) = 0$$

5) (30 points) The following figure shows three different circuits, which are subsystems for a larger system. We can write the transfer functions for these systems as

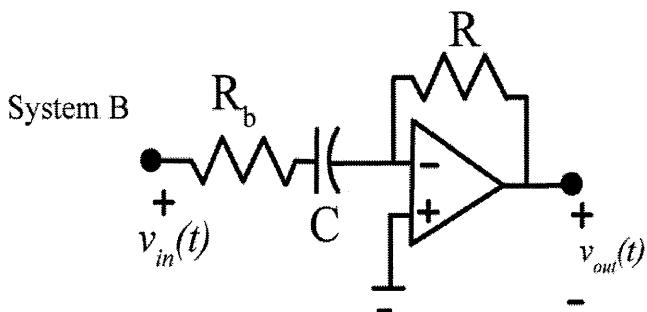
$$G_a(s) = \frac{-K_{low}\omega_{low}}{s + \omega_{low}} \quad G_b(s) = \frac{-K_{high}s}{s + \omega_{high}} \quad G_c(s) = -K_{ap}$$

Determine the parameters K_{low} , ω_{low} , K_{high} , ω_{high} , and K_{ap} in terms of the parameters given (the resistors and capacitors).



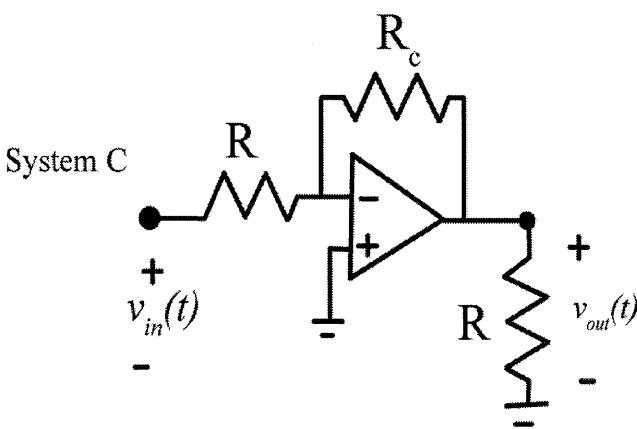
$$\begin{aligned} \frac{V_{in}}{R} + \frac{V_{out}}{R_a} + \frac{V_{out}}{RC} &= 0 \\ -\frac{V_{in}}{R} &= V_{out} \left[\frac{1}{R_a} + CS \right] = V_{out} \left[\frac{R_a C s + 1}{R_a} \right] \\ \frac{V_{out}}{V_{in}} &= -\frac{R_a}{R} \frac{1}{(R_a C s + 1)} = -\frac{R_a / R}{s + 1/R_a C} \\ &= -\frac{R_a / R}{s + 1/R_a C} \end{aligned}$$

$K_{low} = \frac{R_a}{R}$ $\omega_{low} = \frac{1}{R_a C}$



$$\begin{aligned} \frac{V_{in}}{R_b} + \frac{V_{out}}{R} &= 0 \\ \frac{V_{in}}{R_b} \frac{1}{Cs} &= -\frac{V_{out}}{R} \\ \frac{V_{out}}{V_{in}} &= -\frac{R C s}{R_b C s + 1} = -\frac{R C s}{R_b C (s + 1/R_b C)} = -\frac{R}{R_b} s \end{aligned}$$

$K_{high} = \frac{R}{R_b}$ $\omega_{high} = \frac{1}{R_b C}$



$$\begin{aligned} \frac{V_{in}}{R} + \frac{V_{out}}{R_c} &= 0 \\ \frac{V_{out}}{V_{in}} &= -\frac{R_c}{R} \end{aligned}$$

$K_{ap} = \frac{R_c}{R}$