Problem 4.48

Crane Problem – Analytical Solution



The pendulum / cart system is used to model the motion of an overhead crane. If the cart is given a specified acceleration profile of

$$b(t) = \frac{3597e^{x}(1-e^{x})}{(1+e^{x})^{3}} + \frac{3597e^{y}(1-e^{y})}{(1+e^{y})^{3}} \text{ cm/s}^{2}$$

Where

x = -43.5668t + 9.38y = -43.5668t + 31.1633

and 0 < t < 0.9,

Determine the best location of the moveable mass L_{wcg} such that the pendulum angular velocity is zero at t = 0.9 seconds. Note that there will be an unknown force acting in the direction of the cart motion so that the cart experiences the specified acceleration.

pendulum mass	$m_p = 68.5 \text{ g}$
moveable massn	$n_{add} = 88.0 \text{ g}$
Pendulum length	$L_p = 43.2 \text{ cm}$
sensor diameter	$d_{s} = 2.5 \text{ cm}$
moveable weight diameter	$d_{w} = 5.0 \text{ cm}$
pivot to moveable weight cg	L_{wcg}
pivot to pendulum cg	L_{pcg}

Notes:

- Draw the system in a displaced orientation to obtain the governing differential equation. (This is the most important part of the analysis part of this lab).
- Write your resulting non-linear differential equation as:

[something]
$$\ddot{\theta}$$
 + [something else] sin(θ) = [something different] b(t)cos(θ)

When implementing this equation in Maple it should look something like this:

 $diff_eq:=(IGp+IGw+mp*LGp^2+mw*Lw^2)*diff(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t))=\dots(rightheta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+(mp*LGp+mw*Lw)*g*sin(theta(t),t$2)+($

• Maple can numerically solve the non-linear differential equation of motion using: >soln := dsolve({diff_eq, theta(0)=0, D(theta) (0)=0}, theta(t),numeric);

To plot your solution use >odeplot(soln, [t,D(theta)(t)], 0..2, numpoints=300);

Be sure to include >with(plots): at the beginning of your Maple Worksheet. Once your Maple worksheet is working correctly you can vary Lw to find the location where the angular velocity is zero at the end of the acceleration.