## ECE-320, Practice Quiz #4

For problems 1-3, consider a closed loop system with transfer function

$$G_0(s) = \frac{s+a}{s^2 + bs + k}$$

- 1) The sensitivity to variations in k,  $S_k^{G_0}(s)$ , is
- a)  $\frac{k}{s^2 + bs + k}$  b)  $\frac{-k}{s^2 + bs + k}$  c) 1 d)  $\frac{k}{s + a} \frac{k}{s^2 + bs + k}$  e) none of these
- **2)** The sensitivity to variations in b,  $S_b^{G_0}(s)$ , is
- a)  $\frac{-b}{s^2 + bs + k}$  b)  $\frac{-bs}{s^2 + bs + k}$  c) 1 d)  $\frac{b}{s + a} \frac{bs}{s^2 + bs + k}$  e) none of thes
- **3**) The sensitivity to variations in a,  $S_a^{G_0}(s)$ , is
- a)  $\frac{a}{s^2 + bs + k}$  b)  $\frac{-a}{s^2 + bs + k}$  c) 1) d)  $\frac{a}{s + a}$  e) none of these
- 4) Assume we compute the sensitivity of a system with nominal value a = 4 to be

$$S_a^{G_0}(s) = \frac{1}{s+a}$$

For what frequencies will the sensitivity function be less than  $\frac{1}{\sqrt{32}}$ ?

- a)  $\omega < 4 \text{ rad/sec}$  b)  $\omega > 4 \text{ rad/sec}$  c)  $\omega > 16 \text{ rad/sec}$  d)  $\omega < 16 \text{ rad/sec}$  e) none of these
- **5**) Assume we compute the sensitivity of a system with nominal value a = 3

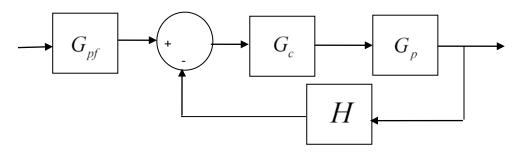
to be

$$S_a^{G_0}(s) = \frac{s+2}{s+1+a}$$

For what frequencies will the sensitivity function be less than  $\sqrt{\frac{10}{16}}$ ?

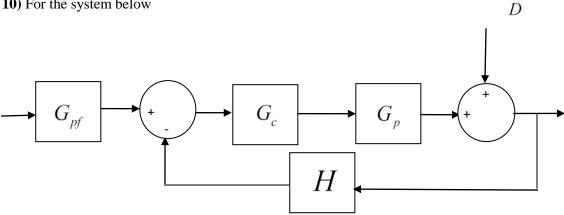
a)  $\omega < 4 \text{ rad/sec b}$ )  $\omega > 4 \text{ rad/sec c}$ )  $\omega > 16 \text{ rad/sec d}$ )  $\omega < 16 \text{ rad/sec e}$ ) none of these

## Problems 6-9 refer to the following system



- **6**) To reduce the sensitivity of the closed loop transfer function variations in the plant  $G_p$  , we should
- a) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  large b) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  small
- c) make  $G_{\it pf}$  large d) do nothing, we cannot change the sensitivity
- 7) To reduce the sensitivity of the closed loop transfer function to variations in the prefilter  $G_{\it pf}$  , we should
- a) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  large b) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  small
- c) make  $G_{pf}$  small d) do nothing, we cannot change the sensitivity
- 8) To reduce the sensitivity of the closed loop transfer function to variations in the controller  $G_c$  we should
- a) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  large b) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  small
- c) make  $|H(j\omega)|$  large d) do nothing, we cannot change the sensitivity
- 9) To reduce the sensitivity of the closed loop transfer function to variations in the sensor H, we should
- a) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  large b) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  small
- c) make  $G_{\it pf}$  large d) do nothing, we cannot change the sensitivity

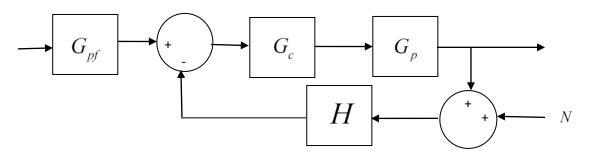
## 10) For the system below



to reduce the effects of the external disturbance D on the system output, we should

- a) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  large b) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  small
- c) make  $G_{pf}$  large d) do nothing, we cannot change the sensitivity

## 11) For the system below



to reduce the effects of sensor noise N on the closed loop system , we should

- a) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  large b) make  $|G_c(j\omega)G_p(j\omega)H(j\omega)|$  small
- c) make  $|H(j\omega)|$  large d) do nothing, we cannot change the sensitivity

- 12) For the 2x2 matrix  $P = \begin{bmatrix} a & b \\ c & d \end{bmatrix}$ , the inverse of this matrix,  $P^{-1}$ , is which of the following:
- a)  $P^{-1} = \frac{1}{ad bc} \begin{bmatrix} a & b \\ c & d \end{bmatrix}$  b)  $P^{-1} = \frac{1}{ad bc} \begin{bmatrix} d & b \\ c & a \end{bmatrix}$  c)  $P^{-1} = \frac{1}{ad bc} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$
- d)  $P^{-1} = \frac{1}{ad + bc} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$  e)  $P^{-1} = \frac{1}{ad + bc} \begin{bmatrix} d & b \\ c & a \end{bmatrix}$  f) none of these
- 13) For the following state variable model

$$\dot{q}(t) = \begin{bmatrix} 1 & 0 \\ 1 & 2 \end{bmatrix} q(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 2 \end{bmatrix} q(t)$$

The poles of the system are at

- a) -1 and -3 b) -2 and -2 c) 1 and 3 d) 0 and 1 e) 1 and 2
- 14) For the following state variable model

$$\dot{q}(t) = \begin{bmatrix} 0 & 1 \\ -1 & -2 \end{bmatrix} q(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 2 \end{bmatrix} q(t)$$

The poles of the system are at

- a) -1 and -2 b) -1 and -1 c) 1 and 3 d) 0 and 1 e) 1 and 2
- 15) For the following state variable model

$$\dot{q}(t) = \begin{bmatrix} -1 & -1 \\ 1 & -3 \end{bmatrix} q(t) + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

$$y(t) = \begin{bmatrix} 1 & 2 \end{bmatrix} q(t)$$

The poles of the system are at

a) -1 and -3 b) -2 and -2 c) 1 and 3 d) 0 and 1 e) -1 and -2

16) Consider the following state variable model

$$\dot{q}(t) = \begin{bmatrix} 0 & 1 \\ 1 & 1 \end{bmatrix} q(t) + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 3 & 0 \end{bmatrix} q(t)$$

Assume state variable feedback of the form  $u(t) = G_{pf}r(t) - Kq(t)$  The closed loop transfer function for this system is which of the following?

a) 
$$G(s) = \frac{-6G_{pf}}{s(s-1+2k_2)+2k_1-1}$$
 b)  $G(s) = \frac{6G_{pf}}{s(s-1+2k_2)+2k_1-1}$ 

c) 
$$G(s) = \frac{6G_{pf}}{s(s-1+2k_2)-2k_1+1}$$
 d)  $G(s) = \frac{-6G_{pf}}{s(s-1+2k_2)-2k_1+1}$ 

17) Consider the following state variable model

$$\dot{q}(t) = \begin{bmatrix} -1 & 2 \\ 0 & 1 \end{bmatrix} q(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u(t)$$
$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} q(t)$$

Assume state variable feedback of the form  $u(t) = G_{pf} r(t) - Kq(t)$  Is the closed loop transfer function for this system equal to

$$G(s) = \frac{G_{pf}}{s+1+k_1}$$

- a) yes b) no
- 18) A system with state variable feedback has the closed loop transfer function

$$G(s) = \frac{8G_{pf}}{s^2 + (k_1 + 12)s + (k_1 + k_2 + 20)}$$

Is this system *controllable*?

- a) Yes b) No c) impossible to determine
- 19) A system with state variable feedback has the closed loop transfer function

$$G(s) = \frac{G_{pf}}{s^2 + (k_1 - 1)s + (k_2 + 2)}$$

Is the system controllable?

a) Yes b) No c) impossible to determine

20) A system with state variable feedback has the closed loop transfer function

$$G(s) = \frac{G_{pf}}{(s - k_1 k_2)^2}$$

Is the system controllable?

- a) Yes b) No c) impossible to determine
- **21**) Consider a plant that is unstable but is a controllable system. Is it possible to use state variable feedback to make this system stable?
- a) Yes b) No

Answers: 1-b, 2-b, 3-d, 4-b, 5-a, 6-a, 7-d, 8-a, 9-b, 10-a, 11-b, 12-c, 13-e, 14-b, 15-b, 16-b, 17-a, 18-a, 19-a, 20-b, 21-a