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## ECE-320 Linear Control Systems Spring 2014, Exam 2

No calculators or computers allowed.

Problem 1	/15
Problem 2	/25
Problem 3	/20
Problem 4	/20
Problem 5	/20
Total	/100

- 1) (15 Points) Consider a system with closed loop transfer function  $G_o(s) = \frac{k_p s}{s + 1 + k_p s}$ . The nominal values for the parameter  $k_p$  is 2.
- a) Determine an expression for the sensitivity of the closed loop system to variations in  $k_p$ . Your final answer should be written as numbers and the complex variable s.
- answer should be written as numbers and the complex variables.

  b) Determine expressions for the <u>magnitude</u> of the sensitivity functions in terms of frequency,  $\omega$

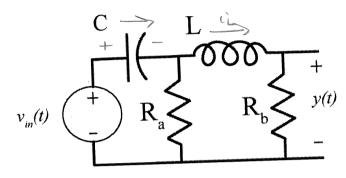
a) 
$$\int_{Kp}^{60} = \frac{Kp}{N} \frac{\partial N}{\partial Kp} - \frac{kp}{D} \frac{\partial D}{\partial Kp}$$

$$= \frac{kp}{Kpk} (k) - \frac{kp}{k+1+kp} (k) = 1 - \frac{kpk}{k+1+kpk} = \frac{k+1}{k+1+kpk}$$

$$\int_{Kp}^{60} = \frac{k+1}{k+1+kpk} = \frac{k+1}{3k+1}$$
b) 
$$\int_{Kp}^{60} (i\omega) = \frac{kp}{q\omega^2 + 1}$$

2) (25 Points) For the following circuit, the state variables are the current through the inductor and the voltage across the capacitor. Determine a state variable model for this system. Specifically, you need to identify the A, B, C, and D matrices/vectors/scalars. You surely recall the useful relationships

$$v(t) = L \frac{di(t)}{dt}, i(t) = C \frac{dv(t)}{dt}$$



$$C\frac{dV_c}{dt} = \frac{V_1 + (V_{in} - V_c)}{R_a}$$

$$\frac{dV_c}{dt} = \frac{-1}{Rac} V_c + \frac{1}{L} \frac{v_i}{v_i} + \frac{1}{L} \frac{v_i}{v_i}$$

$$\frac{dV_c}{dt} = \frac{-1}{L} V_c - \frac{C_c}{L} \frac{v_i}{v_i} + \frac{1}{L} V_{in}$$

$$\frac{d}{dt} \begin{bmatrix} v_c \\ i_L \end{bmatrix} = \begin{bmatrix} -\frac{1}{4} & -\frac{1}{4} \\ -\frac{1}{4} & -\frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} & \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{1}{4} & \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \begin{bmatrix} v_c \\ v_i \end{bmatrix} + \begin{bmatrix} \frac{$$

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3) (20 Points) For the state variable model

$$\dot{q} = \begin{bmatrix} 2 & 0 \\ 2 & 3 \end{bmatrix} q + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 0 & 1 \end{bmatrix} q + \begin{bmatrix} 0 \end{bmatrix} u$$

Determine the closed loop transfer function with <u>state variable feedback</u>,  $u(t) = G_{pf}r(t) - Kq(t)$ 

$$\widetilde{A} = A - BK = \begin{bmatrix} 2 & 0 \\ 2 & 3 \end{bmatrix} - \begin{bmatrix} 0 \end{bmatrix} \begin{bmatrix} K_1 & K_2 \end{bmatrix} = \begin{bmatrix} 2 & 0 \\ 2 - K_1 & 3 - K_2 \end{bmatrix}$$

$$\pm J - \widehat{A} = \begin{bmatrix} \pm -2 & 0 \\ K_1 - 2 & 4 + K_2 - 3 \end{bmatrix}$$

$$($1-A)^{-1} = \frac{1}{($-2)($+$-3)} \begin{bmatrix} $+$ & $-3$ & $0 \\ 2-$ & $-$ & $-2 \end{bmatrix}$$

$$G_{0}(\xi) = C(4J-\widetilde{A})^{-1}\widetilde{B} = [0] \qquad [5+k_{2}-3] \qquad 0 \ [6+2](4+k_{2}-3) \qquad [2-k_{1} \qquad 4-2][6p4]$$

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4) (20 points) For impulse response  $h(n) = \left(\frac{1}{2}\right)^{n+2} u(n-1)$  and input  $x(n) = \left(\frac{1}{4}\right)^{n-3} u(n-2)$ , use z-transforms of the input and impulse response to determine the system output y(n)

*Hint*: Assume  $Y(z) = z^{-2}G(z)$ 

$$H(z) = -2 \left\{ \left( \frac{1}{z} \right)^{n-1} \left( \frac{1}{z} \right)^3 u(n-1) \right\} = \frac{1}{8} z^{-1} \frac{2}{z^{-1/2}} = \left[ \frac{\frac{1}{8}}{z^{-1/2}} = H(z) \right]$$

$$I(2) = 2 \left\{ \left( \frac{1}{4} \right)^{n-2} \left( \frac{1}{4} \right)^{-1} U(n-2) \right\} = 42^{-2} \frac{2}{2-4} = \left[ \frac{43^{-1}}{2-4} = 262 \right)$$

$$Y_{(2)} = \frac{1/2 + 1}{(2 - 1/2)(2 - 1/4)}$$
  $(60) = \frac{1/2 + 2}{(2 - 1/2)(2 - 1/4)}$   $(12) = 2^{-2} (612)$ 

$$\frac{612}{2} = \frac{1}{(2^{-1})(2^{-1})} = \frac{A}{2^{-1}} + \frac{B}{2^{-1}} + \frac{A}{2^{-1}} = 2$$

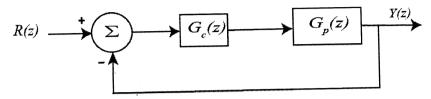
$$B = \frac{1}{2} = -2$$

$$y(n) = g(n-2) = 2[(\frac{1}{2})^{n-2} - (\frac{1}{4})^{n-2}]u(n-2) = y(n)$$

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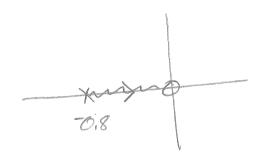
5) (20 points) For the following problem, assume the closed loop system below and assume

$$G_p(s) = \frac{z}{(z+0.8)}$$



Hint: Drawing a root locus plot for a discrete-time system is identical to drawing the root locus plot for a continuous time system (treat z as you would s). The only difference is the interpretation.

a) Assume we are using the controller  $G_c(z) = k$ . Sketch the root locus, including the direction travelled as the gain increases and the angle of the asymptotes and centroid of the asymptotes, if necessary.



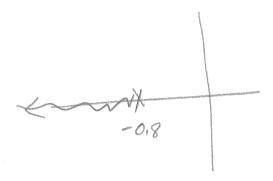
In order for the system to be stable, we should require which of the following conditions (assume  $k_o$  is a suitable chosen positive number)  $k < k_o$   $k > k_o$  k > 0

Assuming the system is stable, will the closed loop system respond faster or slower as k is increased?

faster as pole moves closer to origin

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**b)** Assume we are using the controller  $G_c(z) = kz^{-1}$ . Sketch the root locus, including the direction travelled as the gain increases and the angle of the asymptotes and centroid of the asymptotes, if necessary.



In order for the system to be stable, we should require which of the following conditions (assume  $k_o$  is a suitable chosen positive number)  $k < k_o$   $k > k_o$  k > 0

Assuming the system is stable, will the closed loop system respond faster or slower as k is increased?

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