ECE-320: Linear Control Systems
Homework 3
Due: Thursday March 25 at the beginning of class

## Exam 1, Thursday April 1

1) For the following systems
a) Determine the value of the prefilter gain $G_{p f}$ so that the steady state error for a unit step input of the closed loop system is zero. (Hint: Think about the easiest way to do this, you should never have to write out the closed loop transfer function as the ratio of two polynomials.) Ans. 1,4,1.3,2.5 (though not in that order)
b) Simulate each system in Matlab (not Simulink) for a step response. Run the simulation until the system comes to steady state. Use subplot to put all four plots on one page. You may want to type orient tall before your first plot so Matlab will use more of the page.

2) For a system with the following pole locations, estimate the settling time and determine the dominant poles
a) $-1,-1,-4,-5$
b) $-4,-6,-6,-8$
c) $-1+\mathrm{j},-1-\mathrm{j},-2,-2$
d) $-3-2 \mathrm{j},-3+2 \mathrm{j},-4+\mathrm{j},-4-\mathrm{j}$

Ans. 4/3, 4, 4, 1 (though not in that order)
3) For the following transfer functions, determine

- the characteristic polynomial
- the characteristic modes
- if the system is stable, unstable, or marginally stable
a) $H(s)=\frac{s-1}{s(s+2)(s+10)}$
b) $H(s)=\frac{s(s-1)}{(s+1)^{2}\left(s^{2}+s+1\right)}$
c) $H(s)=\frac{1}{s^{2}(s+1)}$
d) $H(s)=\frac{s^{2}-1}{(s-1)(s+2)\left(s^{2}+1\right)}$
e) $H(s)=\frac{1}{\left(s^{2}+2\right)(s+1)}$

4) Assume we have the following system

where $G_{p}(s)=\frac{1}{s+2}$. We want to design a model matching controller so that

- the closed loop system is a second order
- the state error for a step input is zero
- the settling time of the closed loop system is 3 seconds
- the percent overshoot of the closed loop system is $20 \%$
. You are to determine the closed loop transfer function and then the controller to meet these specifications.
Ans. $\quad G_{c}(s)=\frac{8.53(s+2)}{s(s+2.66)}$

5) Assume we have the following system

where $G_{p}(s)=\frac{1}{s+2}$. We want to design a model matching controller so that

- the closed loop system is a second order
- the steady state error for a step input is zero
- the bandwidth of the closed loop system is 2 Hz .

Luckily I have an uncle who sells good poles cheap, so I obtained a pole at $-10 \pi \mathrm{rad} / \mathrm{sec}$ for your system. You are to determine the closed loop transfer function (i.e., find the other pole and the numerator) and then the controller to meet these specifications.
(Hint: Read Chapter 7 of the notes!, Ans. $G_{c}(s)=\frac{40 \pi^{2}(s+2)}{s(s+14 \pi)}$ )

## Preparation for Lab 3

6) Consider the following model of the two degree of freedom system we will be using in lab 3 .

a) Draw free body diagrams for each mass and show that the equations of motion can be written as

$$
\begin{array}{rlc}
m_{1} \ddot{x}_{1}+c_{1} \dot{x}_{1}+\left(k_{1}+k_{2}\right) x_{1} & =F+k_{2} x_{2} \\
m_{2} \ddot{x}_{2}+c_{2} \dot{x}_{2}+\left(k_{2}+k_{3}\right) x_{2} & =k_{2} x_{1}
\end{array}
$$

If we define $q_{1}=x_{1}, q_{2}=\dot{x}_{1}, q_{3}=x_{2}$, and $q_{4}=\dot{x}_{2}$, then we get the following state equations

$$
\left[\begin{array}{c}
\dot{q}_{1} \\
\dot{q}_{2} \\
\dot{q}_{3} \\
\dot{q}_{4}
\end{array}\right]=\left[\begin{array}{cccc}
0 & 1 & 0 & 0 \\
-\left(\frac{k_{1}+k_{2}}{m_{1}}\right) & -\left(\frac{c_{1}}{m_{1}}\right) & \left(\frac{k_{2}}{m_{1}}\right) & 0 \\
0 & 0 & 0 & 1 \\
\left(\frac{k_{2}}{m_{2}}\right) & 0 & -\left(\frac{k_{2}+k_{3}}{m_{2}}\right) & -\left(\frac{c_{2}}{m_{2}}\right)
\end{array}\right]\left[\begin{array}{c}
q_{1} \\
q_{2} \\
q_{3} \\
q_{4}
\end{array}\right]+\left[\begin{array}{c}
0 \\
\left(\frac{1}{m_{1}}\right) \\
0 \\
0
\end{array}\right] F
$$

This is of the general form $\dot{q}(t)=A q(t)+B F(t)$. In what follows the notation $A_{i, j}$ refers to the entry in the $i^{t h}$ row and $j^{\text {th }}$ column in the above $A$ matrix. In order to get the $A$ and $B$ matrices for the state variable model, we need to determine all of the quantities in the above matrices.
b) Now we will rewrite the equations from part (a) as

$$
\begin{aligned}
\ddot{x}_{1}+2 \zeta_{1} \omega_{1} \dot{x}_{1}+\omega_{1}^{2} x_{1} & =\frac{k_{2}}{m_{1}} x_{2}+\frac{1}{m_{1}} F \\
\ddot{x}_{2}+2 \zeta_{2} \omega_{2} \dot{x}_{2}+\omega_{2}^{2} x_{2} & =\frac{k_{2}}{m_{2}} x_{1}
\end{aligned}
$$

We will get our initial estimates of $\zeta_{1}, \omega_{1}, \zeta_{2}$, and $\omega_{2}$ using the log-decrement method (assuming only one cart is free to move at a time and there are not inputs). Assuming we have measured these parameters, show how $A_{2,1}, A_{2,2}, A_{4,3}$, and $A_{4,4}$ can be determined.
c) By taking the Laplace transforms of the equations from part (b), show that we get the following transfer function

$$
\frac{X_{2}(s)}{F(s)}=\frac{\left(\frac{k_{2}}{m_{1} m_{2}}\right)}{\left(s^{2}+2 \zeta_{1} \omega_{1} s+\omega_{1}^{2}\right)\left(s^{2}+2 \zeta_{2} \omega_{2} s+\omega_{2}^{2}\right)-\frac{k_{2}^{2}}{m_{1} m_{2}}}
$$

d) It is more convenient to write this as

$$
\frac{X_{2}(s)}{F(s)}=\frac{\left(\frac{k_{2}}{m_{1} m_{2}}\right)}{\left(s^{2}+2 \zeta_{a} \omega_{a} s+\omega_{a}^{2}\right)\left(s^{2}+2 \zeta_{b} \omega_{b} s+\omega_{b}^{2}\right)}
$$

By equating powers of $s$ in the denominator of the transfer function from part (c) and this expression you should be able to write down four equations. The equations corresponding to the coefficients of $s^{3}, s^{2}$, and $s$ do not seem to give us any new information, but they will be used to get consistent estimates of $\zeta_{1}$ and $\omega_{1}$.

The equation for the coefficient of $s^{0}$ will give us a new relationship for $\frac{k_{2}^{2}}{m_{1} m_{2}}$ in terms of the parameters we will be measuring.
e) We will actually be fitting the frequency response data to the following transfer function

$$
\frac{X_{2}(s)}{F(s)}=\frac{K_{2}}{\left(\frac{1}{\omega_{a}^{2}} s^{2}+\frac{2 \zeta_{a}}{\omega_{a}} s+1\right)\left(\frac{1}{\omega_{b}^{2}} s^{2}+\frac{2 \zeta_{b}}{\omega_{b}} s+1\right)}
$$

What is $K_{2}$ in terms of the parameters of part (d)?
f) Using the transfer function in (d) and the Laplace transform of the second equation in part (b), show that the transfer function between the input and the position of the first cart is given as

$$
\frac{X_{1}(s)}{F(s)}=\frac{\frac{1}{m_{1}}\left(s^{2}+2 \zeta_{2} \omega_{2} s+\omega_{2}^{2}\right)}{\left(s^{2}+2 \zeta_{a} \omega_{a} s+\omega_{a}^{2}\right)\left(s^{2}+2 \zeta_{b} \omega_{b} s+\omega_{b}^{2}\right)}
$$

g) This equation is more convenient to write in the form

$$
\frac{X_{1}(s)}{F(s)}=\frac{K_{1}\left(\frac{1}{\omega_{2}^{2}} s^{2}+\frac{2 \zeta_{2}}{\omega_{2}} s+1\right)}{\left(\frac{1}{\omega_{a}^{2}} s^{2}+\frac{2 \zeta_{a}}{\omega_{a}} s+1\right)\left(\frac{1}{\omega_{b}^{2}} s^{2}+\frac{2 \zeta_{b}}{\omega_{b}} s+1\right)}
$$

What is $K_{1}$ in terms of the quantities given in part (f)?
h) Verify that $A_{4,1}=\frac{k_{2}}{m_{2}}=\frac{K_{2}}{K_{1}} \omega_{2}^{2}$
i) Verify that $A_{2,3}=\frac{k_{2}}{m_{1}}=\frac{\omega_{1}^{2} \omega_{2}^{2}-\omega_{a}^{2} \omega_{b}^{2}}{A_{4,1}}$
j) Verify that $B_{2}=\frac{1}{m_{1}}=\frac{K_{2} \omega_{a}^{2} \omega_{b}^{2}}{A_{4,1}}$. Note that this term contains all of the scaling and unit conversions.

