

Name SOLUTIONS Mailbox _____

ECE-205

Exam 3

Winter 2013

Calculators and computers are not allowed. You must show your work to receive credit.

Problem 1 _____/15

Problem 2 _____/10

Problem 3 _____/20

Problem 4 _____/15

Problems 5 _____/20

Problems 6 _____/20

Total _____

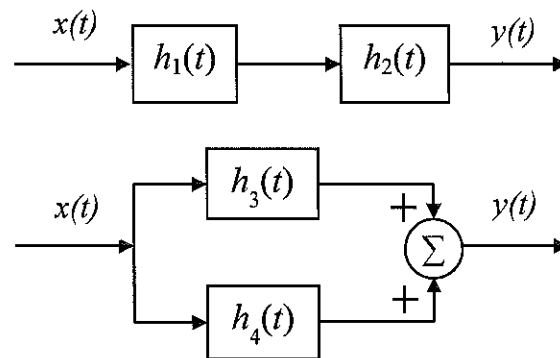
1) (15 Points) Consider the LTI systems with the following impulses responses:

$$h_1(t) = \delta(t-2), \quad h_2(t) = \delta(t-1) - 3\delta(t-3), \quad h_3(t) = e^{(t+1)}\delta(t+1), \quad h_4(t) = u(t-2) - \delta(t+1)$$

i) Fill in the following table. You do not need to show any work.

| | Causal? (Y/N) | BIBO Stable? (Y/N) |
|---------------------------------------|---------------|--------------------|
| $h_1(t) = \delta(t-2)$ | Y | Y |
| $h_2(t) = \delta(t-1) - 3\delta(t-3)$ | Y | Y |
| $h_3(t) = e^{(t+1)}\delta(t+1)$ | N | Y |
| $h_4(t) = u(t-2) - \delta(t+1)$ | N | N |

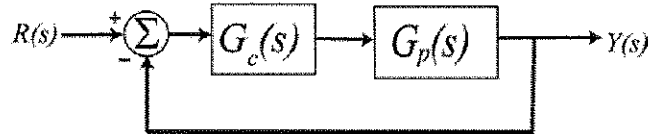
ii) Determine the overall impulse response (the impulse response between input $x(t)$ and output $y(t)$) of the following interconnected systems. You must show your work for a full credit.



$$\begin{aligned}
 h_1(t) * h_2(t) &= \int_{-\infty}^{\infty} \delta(\lambda-2) [\delta(t-\lambda-1) - 3\delta(t-\lambda-3)] d\lambda \\
 &= \int_{-\infty}^{\infty} \delta(\lambda-2) \delta(t-\lambda-1) d\lambda - 3 \int_{-\infty}^{\infty} \delta(\lambda-2) \delta(t-\lambda-3) d\lambda \\
 &= \delta(t-1-2) - 3\delta(t-3-2) = \boxed{\delta(t-3) - 3\delta(t-5)}
 \end{aligned}$$

$$\begin{aligned}
 h_3(t) + h_4(t) &= e^{(t+1)}\delta(t+1) + u(t-2) - \delta(t+1) \\
 &= e^{(-1+1)}\delta(t+1) + u(t-2) - \delta(t+1) \\
 &= \delta(t+1) + u(t-2) - \delta(t+1) \\
 &= \boxed{u(t-2)}
 \end{aligned}$$

2) (10 points) Consider the following simple feedback control block diagram. The plant, the thing we want to control, has the transfer function $G_p(s) = \frac{2}{s+3}$



a) Determine the settling time of the plant alone (assuming there is no feedback)

(Dominant) pole at $s = -3$

$$\Rightarrow T_s = \frac{4}{3}$$

b) Determine the steady state error for plant alone assuming the input is a unit step (simplify your answer as much as possible)

unit step $\Rightarrow A = 1$

$$e_{ss} = A[1 - G_p(0)] = 1 - G_p(0) = 1 - \frac{2}{3} = \frac{1}{3}$$

c) For a proportional controller, $G_c(s) = k_p$, determine the closed loop transfer function $G_o(s)$

$$G_o(s) = \frac{\frac{2k_p}{s+3}}{1 + \frac{2k_p}{s+3}} = \frac{2k_p}{s+3+2k_p}$$

d) Determine the settling time of the closed loop system, in terms of k_p

(Dominant) pole at $s = -(3+2k_p)$

$$\Rightarrow T_s = \frac{4}{3+2k_p}$$

e) Determine the steady state error of the closed loop system for a unit step, in terms of k_p (simplify your answer as much as possible)

unit step input $\Rightarrow A = 1$

$$e_{ss} = A[1 - G_o(0)] = 1 - G_o(0) = 1 - \frac{2k_p}{3+2k_p} = \frac{3}{3+2k_p}$$

3) (20 points) Determine

a) the impulse response of $H(s) = \frac{4}{s^2 + 2s + 5}$

b) the unit step response of $H(s) = \frac{e^{-2s}}{(s+1)^2}$

a)

$$H(s) = \frac{4}{s^2 + 2s + 5} = \frac{4}{(s+1)^2 + (2)^2} = \left(\frac{2}{(s+1)^2 + (2)^2} \right) \cdot 2$$

Completing the square

by: $\mathcal{L}\{e^{-\alpha t} \sin(\omega_0 t) u(t)\} = \frac{\omega_0}{(s+\alpha)^2 + \omega_0^2}$

$$\Rightarrow \boxed{h(t) = 2e^{-t} \sin(2t) u(t)}$$

b) Unit step input $x(t) = u(t) \leftrightarrow X(s) = 1/s$
 Unit step response $Y(s) = H(s)X(s) = \frac{1}{s} H(s) = \frac{e^{-2s}}{s(s+1)^2}$

Let $G(s) = \frac{1}{s(s+1)^2}$

By partial fractions:

$$G(s) = \frac{1}{s(s+1)^2} = \frac{A}{s} + \frac{B}{s+1} + \frac{C}{(s+1)^2}$$

• By cover-up method: $A=1, C=-1$

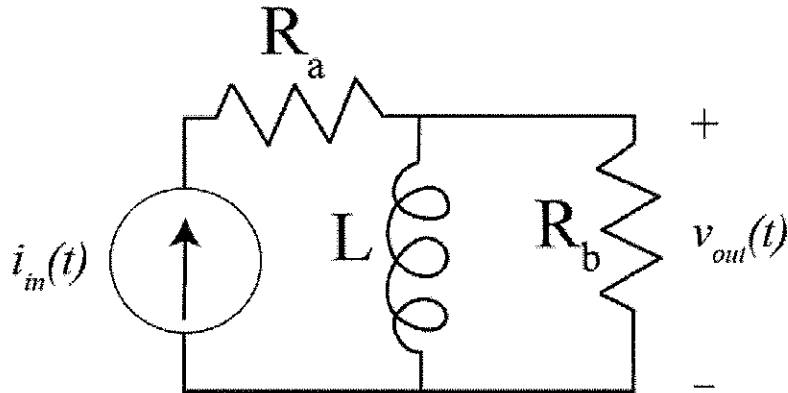
• multiply by s and taking $s \rightarrow \infty$: $0 = A+B \Rightarrow B=-1$

$$\Rightarrow G(s) = \frac{1}{s} - \frac{1}{s+1} - \frac{1}{(s+1)^2} \leftrightarrow g(t) = u(t) - e^{-t} u(t) - t e^{-t} u(t)$$

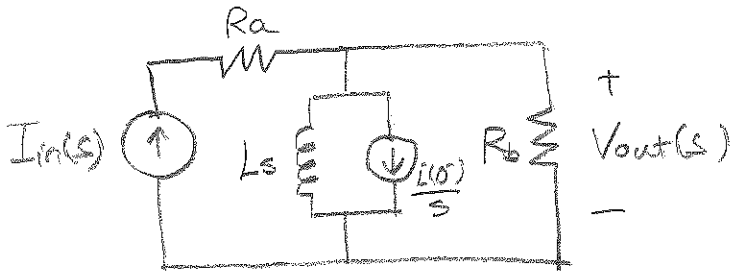
Finally, $Y(s) = e^{-2s} G(s) \leftrightarrow y(t) = g(t-2)$

$$\therefore \boxed{y(t) = [1 - e^{-(t-2)} - (t-2)e^{-(t-2)}] u(t-2)}$$

4) (15 points) For the following circuit



- Determine the ZIR
- Determine the ZSR
- Determine the transfer function



$$I_{in}(s) = \frac{V_{out}(s)}{Ls} + \frac{i(0^-)}{s} + \frac{V_{out}(s)}{R_b}$$

$$\Rightarrow V_{out}(s) = + \frac{R_b L s}{Ls + R_b} I_{in}(s) - \frac{R_b L}{Ls + R_b} i(0^-)$$

$$= + \underbrace{\frac{R_b \cdot s}{s + R_b/L} I_{in}(s)}_{\text{ZSR}} - \underbrace{\frac{R_b}{s + R_b/L} i(0^-)}_{\text{ZIR}}$$

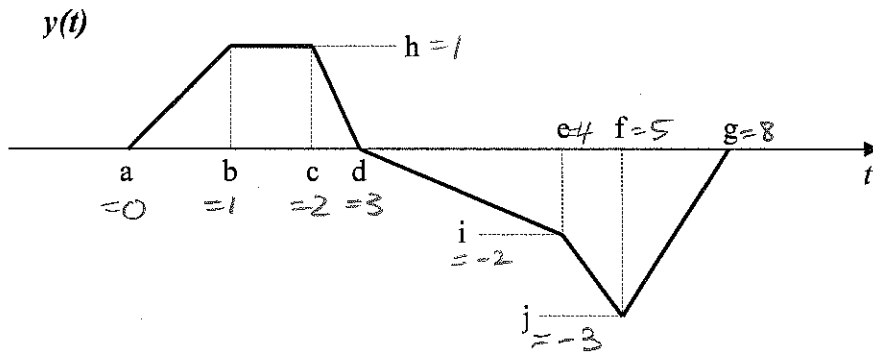
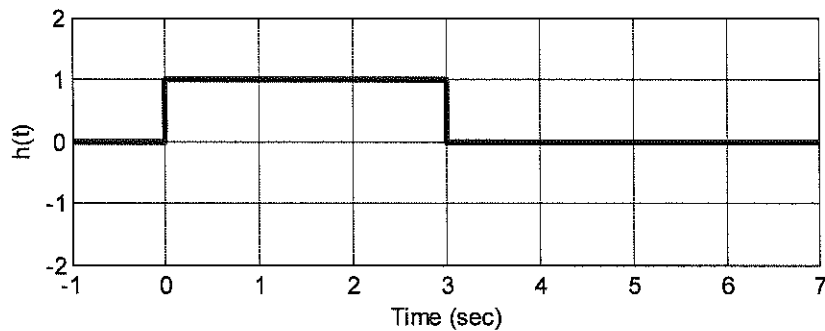
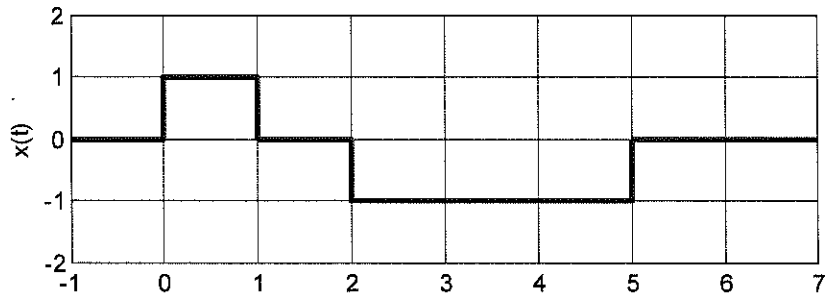
$$\begin{aligned} \text{ZIR} &= - \frac{R_b}{s + R_b/L} i(0^-) \\ \text{ZSR} &= + \frac{R_b \cdot s}{s + R_b/L} I_{in}(s) \end{aligned}$$

Transfer Function:

$$H(s) = \frac{V_{out}(s)}{I_{in}(s)} = + \frac{R_b \cdot s}{s + R_b/L}$$

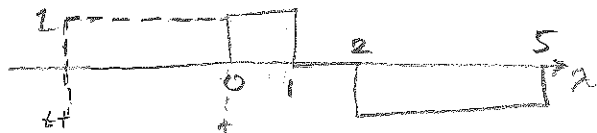
5) (20 Points) An LTI system has input, impulse response, and output as shown below. Determine numerical values for the parameters $a-j$. Note that parameters $a-g$ correspond to *times*, and $h-j$ correspond to *amplitudes*.

Note that the output graph is only an approximate sketch of the output. Do not try to read values from this sketch.



a) $t=0 \Rightarrow a=0$

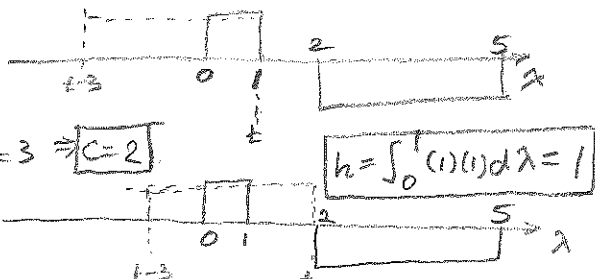
d) $t=3 \Rightarrow d=3$



b) $t=2 \Rightarrow b=1$

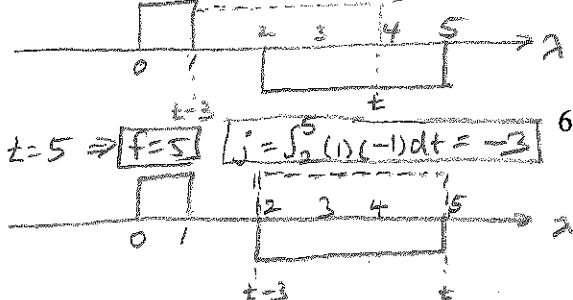


e) $t=4 \Rightarrow e=4$ $i = \int_2^4 (1)(-1) dt = -2$



c) $t=3 \Rightarrow c=2$

$h = \int_0^1 (1)(1) d\lambda = 1$

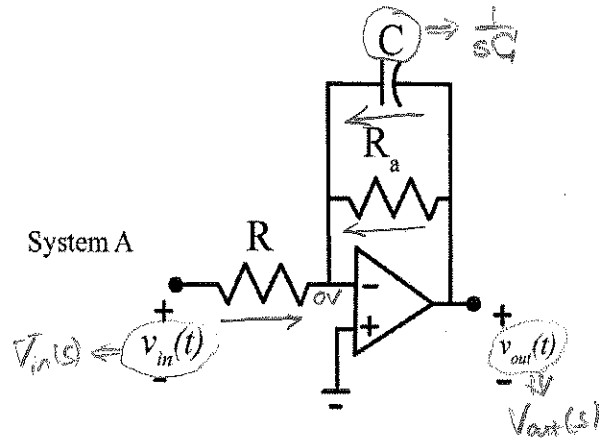


f) $t=5 \Rightarrow f=5$ $j = \int_2^5 (1)(-1) dt = -3$

6) (20 points) The following figure shows three different circuits, which are subsystems for a larger system. We can write the transfer functions for these systems as

$$G_a(s) = \frac{-K_{low}\omega_{low}}{s + \omega_{low}} \quad G_b(s) = \frac{-K_{high}s}{s + \omega_{high}} \quad G_c(s) = -K_{ap}$$

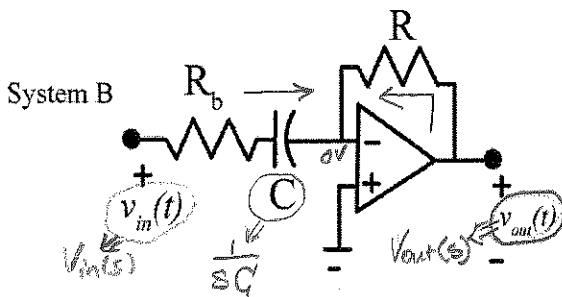
Determine the parameters K_{low} , ω_{low} , K_{high} , ω_{high} , and K_{ap} in terms of the parameters given (the resistors and capacitors).



$$\frac{V_{in}(s)}{R} + \frac{V_{out}(s)}{R_a} + \frac{V_{out}(s)}{1/sC} = 0$$

$$\Rightarrow \frac{V_{out}(s)}{V_{in}(s)} = \frac{-1/(RC)}{s + 1/(RC)}$$

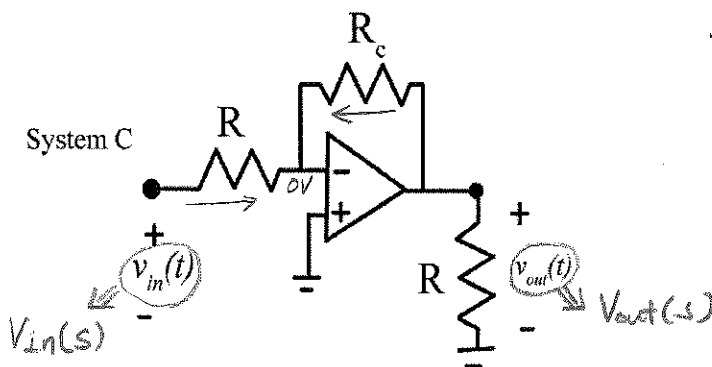
$$\Rightarrow \boxed{K_{low} = R_a/R}, \quad \boxed{\omega_{low} = 1/(RC)}$$



$$\frac{V_{in}(s)}{R_b + 1/sC} + \frac{V_{out}(s)}{R} = 0$$

$$\Rightarrow \frac{V_{out}(s)}{V_{in}(s)} = -\frac{RCs}{R_bCs + 1} = -\frac{(R/R_b)s}{s + 1/(R_bC)}$$

$$\Rightarrow \boxed{K_{high} = R/R_b}, \quad \boxed{\omega_{high} = 1/(R_bC)}$$



$$\frac{V_{in}(s)}{R} + \frac{V_{out}(s)}{R_c} = 0$$

$$\Rightarrow \frac{V_{out}(s)}{V_{in}(s)} = -\frac{R_c}{R}$$

$$\Rightarrow \boxed{K_{ap} = \frac{R_c}{R}}$$

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