

ECE250 (KEH) BJT Formula Sheet (For Test 2)

BJT Modes of Operation:	Cutoff	BE junction off, BC junction off
	Forward Active	BE junction on, BC junction off
	Reverse Active	BE junction off, BC junction on
	Saturation	BE junction on, BC junction on

For NPN BJT: I_e referenced flowing OUT of BJT, I_b and I_c both referenced flowing INTO BJT
 $V_{be_{ON}} = 0.7\text{ V}$, $V_{ce_{SAT}} = 0.1\text{ V}$

For PNP BJT: I_e referenced flowing INTO BJT, I_b and I_c both referenced flowing OUT OF BJT
 $V_{eb_{ON}} = 0.7\text{ V}$, $V_{ec_{SAT}} = 0.1\text{ V}$

For forward active NPN and PNP BJTs:

$$I_e = I_b + I_c \quad \alpha = \frac{I_c}{I_e} \quad (0 < \alpha < 1) \quad \beta = \frac{I_c}{I_b} = \frac{\alpha}{1 - \alpha}$$

$$r_{\pi} = \frac{n \cdot V_T}{I_{bQ}} \quad r_o = \frac{V_A}{I_{cQ}} \quad g_m = \frac{i_c(t)}{v_{be}(t)} = \frac{\beta}{r_{\pi}}$$

DC Q Point Stability Design Rules of Thumb: $(1 + \beta)R_e = 10R_{TH}$ and $V_{Re} = 1\text{ V}$

General Voltage Amplifier AC Model: $A_{vo} = \left(\frac{v_{out}(t)}{v_{in}(t)} \right)$ $R_{in} = \frac{v_{in}(t)}{i_{in}(t)}$ $R_{out} = \left(\frac{v_{test}}{i_{test}} \right)$ **$v_{in}(t) \rightarrow 0$**
RL = infinity

For CE Amplifier: (Note, you must know how to derive these, if asked on the test)

$$A_{vo} = \frac{-\beta \cdot \frac{R_c \cdot r_o}{R_c + r_o}}{r_{\pi} + (\beta + 1) \cdot R_{e1}} \quad R_{in} = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{r_{\pi} + (\beta + 1) \cdot R_{e1}}} \quad R_{out} = \frac{R_c \cdot r_o}{R_c + r_o}$$

DC Load Line: I_c intercept = $(V_{cc} - V_{ee}) / (R_c + R_e)$ V_{ce} intercept = $V_{cc} - V_{ee}$ Slope = $-1 / (R_c + R_e)$

Note: $V_{ee} = 0$ in a single-ended dc power supply

AC Load Line Slope = $-1 / ([R_c // r_o // R_L] + R_{e1})$ **Note: R_{e1} is unbypassed portion of R_e**

For CC (Emitter Follower) Amplifier: (Note, you must know how to derive these, if asked on the test)

$$A_{v_o} = \frac{(\beta + 1) \cdot \left(\frac{R_e \cdot r_o}{R_e + r_o} \right)}{r_{\pi} + (\beta + 1) \cdot \left(\frac{R_e \cdot r_o}{R_e + r_o} \right)} \quad R_{bin} = r_{\pi} + (\beta + 1) \cdot \frac{1}{\frac{1}{R_e} + \frac{1}{r_o} + \frac{1}{R_L}} \quad R_{in} = \frac{1}{\frac{1}{R_{bin}} + \frac{1}{R_1} + \frac{1}{R_2}}$$

$R_{out} = (R_e // r_o) // (r_{\pi} + R_1 // R_2 // R_s) / (\beta + 1)$ **NOTE: For " $R_{in_no_R_L}$ ", leave R_L out of the R_{bin} formula.**

AC Load Line Slope = $-1 / (R_e // r_o // R_L)$

General Voltage Amplifier Model Voltage, Current, Power Gains:

$A_v = v_{out}/v_s = R_{in} / (R_s + R_{in}) \cdot A_{vo} \cdot R_L / (R_{out} + R_L)$ **Note: For " A_v " of CC Amp, replace R_{in} by $R_{in_no_RL}$**

$$A_i = \frac{i_{out}}{i_{in}} = \frac{\left(\frac{v_{out}}{R_L} \right)}{\left(\frac{v_s}{R_s + R_{in}} \right)} = A_v \cdot \frac{R_s + R_{in}}{R_L} \quad A_p = \frac{P_{out}}{P_{in}} = \frac{v_{out} \cdot i_{out}}{v_s \cdot i_{in}} = A_v \cdot A_i$$